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An Integrated Analysis for Post Hydraulic Fracturing Production Forecast in Conventional Oil Sand Reservoir

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Abstract

Hydraulic fracturing is one of the stimulation treatment in oil and gas well by creating a fractured through a proppant injection to the formation. A most critical problem in the actual oil and gas industry is that the fracturing engineers could not forecast approximately post-production performance after fracturing the job, which is a severe problem. This problem phenomenon has occurred in some cases and significantly impacts production such as oversizing or lower sizing of pumping rate setting. Integrated analysis for post job hydraulic fracturing production based on the geometry model iteration and Productivity Index (PI) comparison in the conventional oil sand reservoir is simply a method to analyze and forecast approximately incremental production performance. The fractured software generates a fractured geometry model that considers half-length of fractured parameters, width in front of perforation, average width, fractured height, and pressure net. Then we compare the Productivity Index's prediction value through the method of Cinco-Ley, Samaniego and Dominguez. A case study in the well of TM#2 (conventional oil sand reservoir) was conducted as the comprehensive study to provide the data and proceed analysis for production forecast. We found that the geometry model and iteration of PKN 2D method generated a small fractured geometry model compare to fracCADE software. The cooperation between PKN 2D method and Cinco-Ley, Samaniego, and Dominguez concept successfully predict post-production forecast. This concept could be proposed as a quick look measurement for production scenarios to overcome pump sizing.

INTRODUCTION

Hydraulic fracturing is a stimulation treatment in oil and gas by creating fractures through a proppant injection to the formation. A most critical problem in actual oil and gas industry is the fracturing engineers could not forecasting approximately post-production performance after fracturing job, consequently the severe problem (Ghosh et al., 2019; Liu et al., 2013). This problem phenomenon has occurred in some cases and significantly impacts production, such as oversizing or lower pumping rate settings (Montgomery & Smith, 2010). The decision to execute hydraulic fracturing in the oil sand reservoir based on the depletion of production performance history. Before hydraulic fracturing, the average oil rate was about 200-230 BOPD. However, the trend of production indicated that the production would decrease incisively. Another treatment has also been proposed for this formation with the mixed result, mainly by using thermal (Afdhol et al., 2020; Ferizal et al., 2013; Hidayat & Abdurrahman, 2018; Kusumastuti et al., 2019; Melysa, 2016). Based on this situation, the hydraulic fracturing option is the correct decision to increase production performance and do skin by-pass in the well target.

This paper presented a study case to enrich the concept and directly illustrate a calculation revealed in this paper. This paper's principal objective is to demonstrate and introduce and show an idea widely about the simple concept of geometry model iteration and productivity index (PI) comparison in a conventional sand oil reservoir. This method analyses and forecasts approximately the incremental production performance (PI) and overtake a pump sizing problem that commonly occurs.

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HYDRAULIC FRACTURING EXECUTION IN TM#2

Hydraulic fracturing was done on well TM#2. Well TM#2 is located in Bekasap Formation in Basin of Middle Sumatera. The reservoir has the characteristic such as dominated by sandstone formation, which has the average reservoir temperature in 200-230 Â°F, the reservoir pressure is 868 psig, mid perforation in 5,532.5 ft, bubble point pressure is 80 psig, API oil in 33, oil viscosity in 3.4 cp and formation volume factor of oil (Bo) in 1.15 bbl/STB.

The comprehensive step of hydraulic fracturing execution in TM#2 was successfully done. It consists of several stages: injectivity test, mini fall-off test, step down test, mini frac, and main frac. Each test has a specific purpose and related to each other. After those tests were successfully done, we can proceed with the production forecasting after fracturing. Several data are required to support and proceed with the calculation such as geomechanics properties, fractured geometry data, fractured fluid properties, injection rate, and formation properties. PKN 2D method was the concept used for the fractured model approximation (Xf >Hf) (Kovalyshen & Detournay, 2010; Rahman & Rahman, 2010). After the error value less than 0.0001, the geometry value from iteration could calculate the PI prediction and compare it by software geometry result.

The decision of execution hydraulic fracturing in TM#2 well based on the depletion of production performance history. Execution of hydraulic fracturing in TM#2 was conducted to design and accomplished the following test:

1. Injectivity Test

This test's main purposes is predicting the capability of formation to be fractured through an injection of frac fluid. This test completed by KCL 2% added by water. The result of the injectivity test shown in Figure 1. This test gives parameters as follows: Surface ISIP = 1,848 psi; Treating Pressure Break = 2,600 psi. According to Economides & Nolte (2000), Instantaneous shut-in pressure (ISIP) is the bottom hole injection pressure immediately after the pump has been shut down. The effect of all the fluid friction-based pressure losses. Treating pressure break is the value where the pressure break formation in stable rate injection.

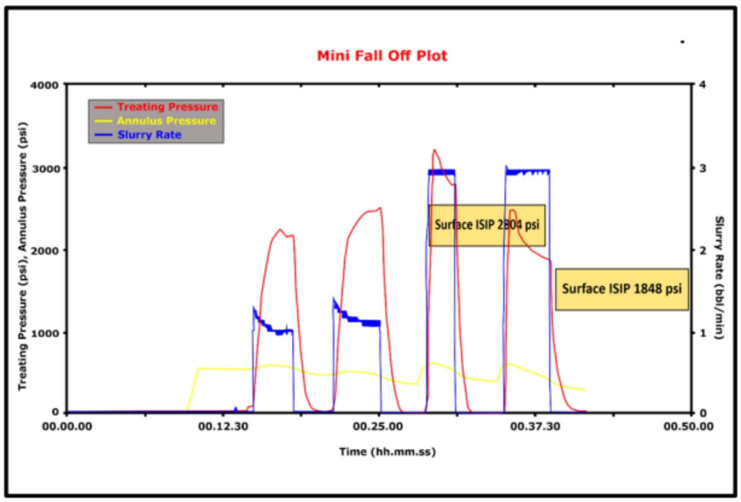

Figure 1. Well TM#2 Injectivity Test

2. Mini fall-off Test

This test is still related to the previous test. The main objective of this test is to predict the transmissibility. This test was conducted by analysis of pressure depletion behaviour. Transimibility is the formation's ability to flow the fluids in certain thickness formation and certain viscosity. Besides those, two additional information could be reached from this test: closure pressure and fracture gradient. Closure pressure is defined as the fluid pressure at which an existing fracture globally closes, and the fracture gradient is defined as the gradient where the fractured could propagate. The test shown in Figure 2 and the result are as follows: Closure pressure = 3720 psi; Fracture gradient = 0.72 psi/ft; Transimibility = 350.14 mD ft/cp.

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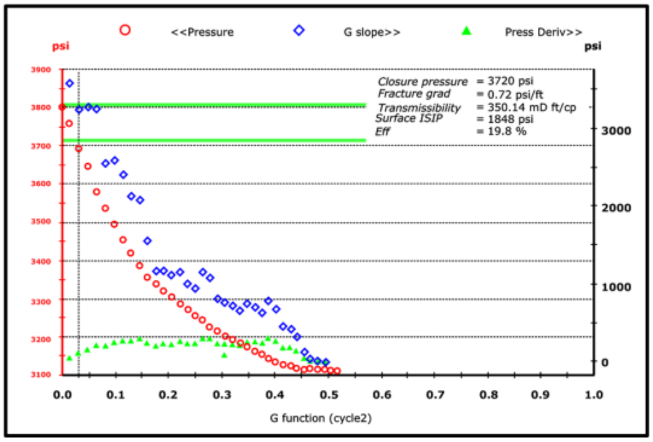

Figure 2. Well TM#2 Mini Fall-off Analysis

3. Step-Rate Test

This test consists of two parts, the first one when pressure gradually increases at a specific rate against time named step (up) rate test. This test run by injection of KCL 2% added water. Another one when pressure decreases gradually against time, called step down test. The step rest test has an objective to predict the fracture extension rate and fracture extension pressure. Fracture extension rate is defined as the rate level that makes fractured propagate, and for fracture extension pressure is defined as the pressure level that makes fractured propagate. Another information that could be gained from this test is to validate closure pressure. For the step-down test, the data collected are analysis perforation friction, tortuosity, and total near-wellbore friction. After the test was conducted and the total near-wellbore pressure plotting against rate, the graph is indicating dominant tortuosity effect. Figure 3 shows the step rate test result. Figure 4 illustrate the plot for domination or perforation effect. The result of this test generate information as follows:

- Frac extension rate = 3.2 bpm
- Frac extension pressure = 3792 psi
- Validate Closure pressure = 3639 psi
- Perforation friction = 350 psi
- Tortuosity = 1300 psi
- Total Near Well Bore Fric = 1650 psi

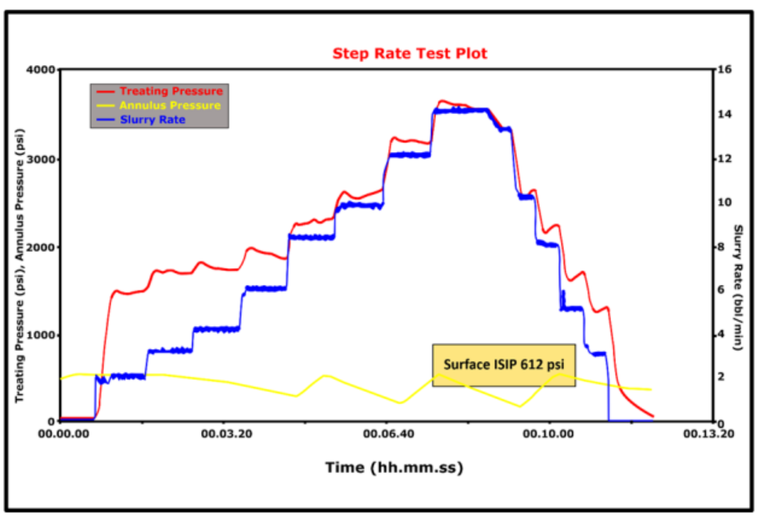

Figure 3. Well TM#2 Step Rate Test

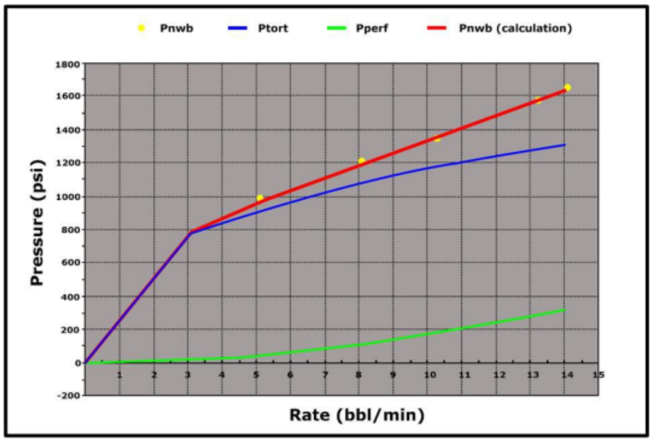

Figure 4. Well TM#2 Analysis for Near Well Bore Effect

4. Mini Frac Test

The main purposes of this test is to make a small scale fractured model before the real main frac is executed. This test was conducted by fluid frac named YF-130 HTD. From this test, fracture engineers are able to make scenario pad design for main fracturing input data. The graph of this test could be seen in Figure 5 and for the result as follows:

- Closure pressure = 2349 psi
- Frac gradient = 0.46 psi/ft
- Leak off Coefficient = 5E-3 ft/min^0.5
- Efficiency = 19.8 %
- Net pressure = 485 psi

Leak off coefficient is defined as the value of how much the effectiveness frac fluid could make a fractured in formation. The efficiency is defined as the comparison between volume fluid injection to the total volume of fracture. Net pressure is defined asthe excess pressure in the fracturing fluid inside the fracture, above that required to simply keep the fractured open[1]and for the design pad scenario and final pad scenario attached in Appendix-1. The graph result of mini frac shown in Figure 5.

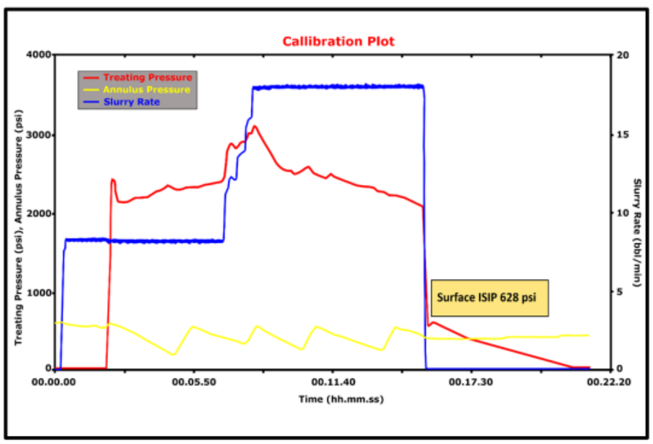

Figure 5. Well TM#2 Mini Frac Test

5. Main Frac

After all data have been collecting and several parameters have been analysis, we could able to conduct a main frac. In this execution the frac fluid that was used called YF 130 HTD. For proppant size 20/40 Carbolite and 12/18 Bauxite have been pumped in this step. The 20/40 Carbolite pumped firstly, then continued by 12/18 Bauxite in order to avoid flow back proppant. During this operation, annulus pressure was constant maintain in range 250-500 psi to balance the differential injection pressure. The test's graph of this test could

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be seen in Figure 6 and the geometry profile shown in Figure 7. Geometry fractured sized that generated as follows:

- Fractured height (Hf) = 32.85 m = 107.8 ft
- Half Length (Xf) = 80.19 m = 263.1 ft
- Average Width ($\bar{w}$) = 0.002794 m = 0.11 inch
- Frac Conductivity (Wkf) = 2108.3 mD-m = 6917 mD-ft

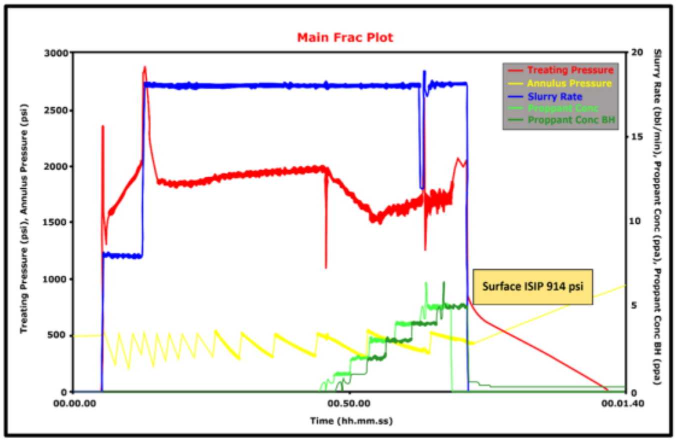

Figure 6. Well TM#2 Main Frac Execution

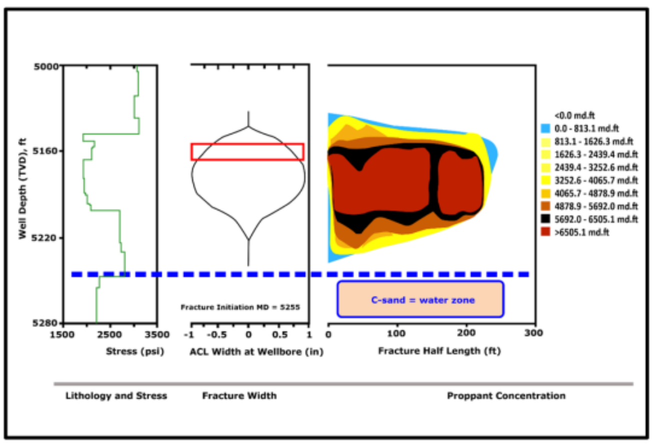

Figure 7. Well TM#2 Geometry Profile against Wkf

RESULTS AND DISCUSSION

The geometry model iteration aims to generate a secondary geometry profile mathematically. The model that used in calculation is PKN 2D model (Due of Xf > Hf), if values of Xf< Hf, it uses KGD 2D model for the calculation[2]. Then we could compare the geometry from software fracCADE 3D to PKN 2D model, and finally proceeding it to PI (Productivity Index) comparison by Method Cinco-Lee, Samadiego, and Domiquez in order for production forecasting. Several data that mentioned in post job report (attached in Appendix-2) require for the calculation proceeding as mentioned in Table 1 and Table 2, respectively.

Table 1. Data Input for Geometry Model Iteration

Parameter Data	Field Unit	Conversion
Young Modulus (E)	1729000 psi	-
Poisson Ratio	0.25	-

n’ base gel	0.4	-
K’ base gel	0.35	-
Rate injection (q_i)	18 bpm	0.046 m^3/second
Total treatment time (T_i)	72 min	4320 second
Spurt loss (S_p)	0 gal/100ft^2	0 m^3/m^2
Coeff. Leak-off total (C_L)	0.0035 ft/√min	0.0001377 m/√sec

Table 2. Geometry Properties Comparison

Parameters	Unit	Well TM#2	
		Design	Actual
Half Length (x_f)	m	49.07	80.19
Average Width ($\bar{w}$)	m	0.00731	0.002794
Fractured Height (h_f)	m	38.1	32.85

The following step of geometry model iteration calculation are:

1. Calculating *Plain Strain Modulus* (E’) as below:

$$E' = \frac{E}{\left(1 - v^2\right)}$$

$$= \frac{1729000}{\left(1 - 0{,}25^2\right)}$$

= 1,844,266.66 psi

2. Determining start for iteration. The value of ($X_{f(iterasi)}$) = 49,07 m. This value is used to be start point in case could penetrate the interest zone as far as 49.07 m.
3. Calculate the width in front of perforation ($w_{(0)}$) through:

$$w_{(0)} = 9.15^{\frac{1}{(2n'+2)}} \times 3.98^{\frac{n'}{(2n'+2)}} \left[\frac{1+2.14n'}{n'}\right]^{\frac{n'}{(2n'+2)}} \times K'^{\frac{1}{(2n'+2)}} \left[\frac{q_i^{n'}.h_f^{(1-n')}.x_f}{E'}\right]^{\frac{1}{(2n'+2)}}.$$

$$= 9{,}15^{\frac{1}{(2(0{,}4)+2)}} \times 3{,}98^{\frac{0{,}4}{(2(0{,}4)+2)}} \left[\frac{1+2{,}14(0{,}4)}{0{,}4}\right]^{\frac{0{,}4}{(2(0{,}4)+2)}}$$

$$\times 0{,}3515^{\frac{1}{(2(0{,}4)+2)}} \left[\frac{0{,}18^{0{,}4} \times 38{,}1^{(1-0{,}64)} \times 49{,}07}{3730689{,}141}\right]^{\frac{1}{(2(0{,}4)+2)}} = 0.063212135 \text{ m}$$

4. Calculatethe average width ($\bar{w}$) through as below:

$\bar{w}$ = π/5 $w_{(0)}$

= (0,2) x (3,14) x (0,063212135) = 0.039697221 m

5. Calculatevalue of β through the equation as below:

$$\beta = \frac{2C_L\sqrt{\pi t}}{\bar{w} + 2S_p}$$

$$= \frac{2(0{,}0001377)\sqrt{(3{,}14)(4320)}}{(0{,}039697221)+2(0)}$$

= 0.807998453

Through Table 4 in Appendix-3 for β = 0.807998453 The value for

$$\left[\exp(\beta^2)erfc(\beta) + \frac{2\beta}{\sqrt{\pi}} - 1\right]$$

= 0.383753

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6. Calculate $X_{f(iterasi+1)}$ through equation as below:

$$x_f = \frac{\left(\bar{w}+2S_p\right)q_i}{4\pi h_f C_L^2}\left[\exp(\beta^2)erfc(\beta)+\frac{2\beta}{\sqrt{\pi}}-1\right]$$

$$= \frac{(0{,}039697221+2(0))(0.046)}{4(3{,}14)(38{,}1)(0.0001377)^2}(0{,}383753)$$

$$= 77.230 \text{ m}$$

7. Calculate the error value through as below:
   Error = $X_{f(iterasi+1)}$ - $X_{f(iterasi)}$

   = 77.230– 49.07

   = 28.16 m

If the error value > 0,0001, the calculation must repeat with the value of $X_{f(iterasi+1)}$ to be plot as $X_{f(iterasi)}$. Theses process continually proceed until reach error value ≤ 0,0001.[4] The table of iteration and trial error process of PKN 2D for Well TM#2 is attached in Appendix-4. For the final result of geometry model iteration are mentioned as below:

- Half Length (X_f)= 69.95671953m = 229.516 ft
- Width in front of perforation $w_{(0)}$= 0.071747 m = 2.824 inch
- Average width ($\bar{w}$)= 0.0450572 m = 1.7739 inch
- Fractured height (h_f)= 38.1 m = 125 ft (*software*)
- Calculate P_{net} through equation as below:

$$P_{net} = \Delta P_f = \frac{E'\left(w_{(0)}\right)}{2hf}$$

$$= \frac{1{,}844{,}266.67\ (0.072)}{2(3.81)}$$

$$= 1736.5 \text{ psi}$$

Then the final comparison of geometry properties through three result that consist of Design, Actual, and PKN 2D Method are mentioned in Table 3.

Table 3. Final Geometry Properties Comparison (Design, Actual, and PKN 2D Method)

Parameter	Unit	Well TM#2		
		Design	**Actual**	**PKN 2D**
Half Length (x_f)	m	49.07	80.19	69.95
Average Width ($\bar{w}$)	m	0.00731	0.00279	0.045057
Fractured Height (h_f)	m	38.1	32.85	38.1

Productivity Index (PI) Prediction Comparison

Productivity Index (PI) is the index value to classified the capability of formation to produce the fluid. Based on theory, the PI will incisively increase after hydraulic fracturing successfully done due to the increase of fractured permeability, frac well radius (rw') and skin by-pass impact on reservoir as shown in Figure 8.

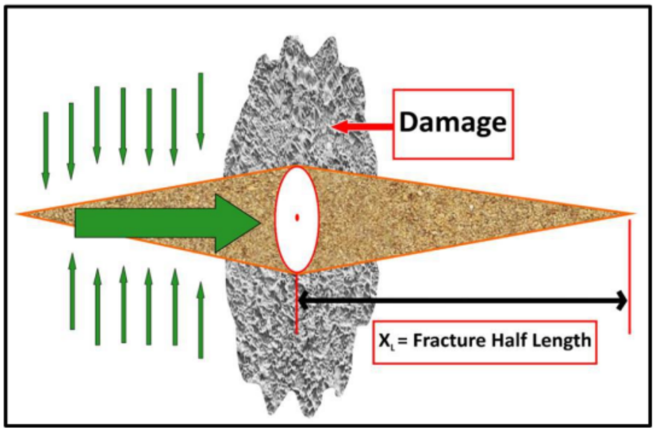

Figure 8. Schematic Fractured Model in Reservoir(3)

The following step will provide the calculation of comparison PI (J/Jo) before and after fracturing using the method of Cinco-Ley, Samaniego and Dominiquez. Then will be followed by IPR Calculation. For the data that requires to proceeding the calculation will be mentioned in Table 4 and Table 5.

Table 4. Input Data for PI Prediction Comparison

Parameter	Unit	Well TM#2
Fractured Conductivity, (Wkf)	mD.ft	6917
Initial Permeability, (ki)	mD	30
Actual Half Length Frac, (Xf)	ft	263.1
Drainage Radius, (re)	ft	570
Well Radius, (rw)	ft	0.3

Table 5. Production Data for IPR Calculation

Production Data	Well TM#2	
	Before HF	After HF
Fluid Rate (Q_L),BFPD	160	430
Oil Rate (Qotest), BOPD	155.74	401.62
Water Rate (Qw), BWPD	4.25	28.38
Gas Rate (Qg), MSCF	0	0
Water cut (WC), %	2.66	6.66
Reservoir Pressure (Pr), psig	818	818
BHP (Pwf test), psi	110	150
Bubble Point Pressure (Pb), psig	80	80
Bo, (BBL/STB)	1.15	1.15
μo, cp	3.4	3.4

The following step of PI prediction calculation are:

1. Fractured Conductivity (Fcd) Calculation
   Fractured conductivity (Fcd) is simply defined as the value of how the capability level to flow fluid in fractured. The calculation as below:

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$$Fcd = \frac{Wkf}{kixXf}$$
$$= \frac{6917}{30x263.1} = 0.8763$$

Then find the effective well radius (rw') by make an intersection perpendicularly in line X for Fcd towards line Y for rw'/Xf through Cinco-Ley, Samaniego and Dominiquez chart as Figure 9. From chart, we have the value for rw'/Xf is 0.19.

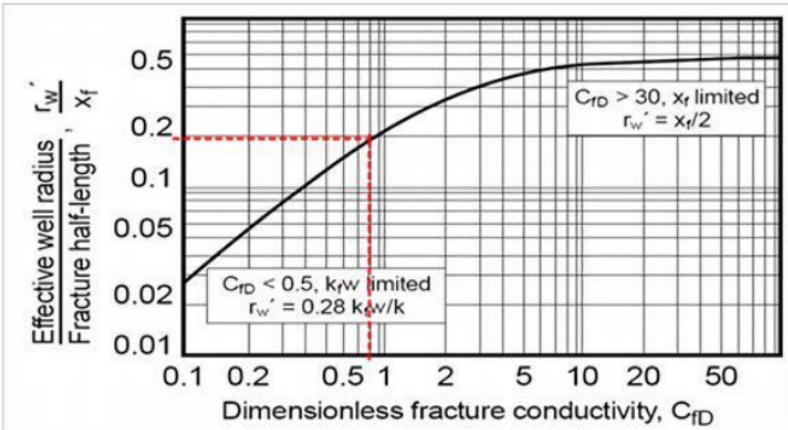

Figure 9. Chart for Fcd vs rw'/Xf Plot

2. Calculation for Comparison of J/Jo (=Initial PI/ Frac PI)
   a. Based on Actual Fractured (Software FracCADE 3D)
      Based on chart where rw'= 0.19 x Xf
      where the actual fractured for Xf = 263.1 ft
      Then rw' = 0.19 x 263.1 ft = 49.98 ft
      Where

$$J / Jo = \frac{\ln(re / rw)}{\ln(re / rw')}$$
$$= \frac{\ln(570 / 0.3)}{\ln(570 / 49.98)}$$
$$= 3.10$$

   b. Based on PKN 2D Method
      Based on chart where rw'= 0.19 x Xf
      where the PKN 2D for Xf = 229.516 ft = 69.95 m
      Then rw' = 0.19 x 229.516 ft = 43.60 ft
      Where

$$J / Jo = \frac{\ln(570 / 0.3)}{\ln(570 / 43.60)}$$
$$= 2.93$$

   c. Based on Production History
      Where

$$J / Jo = \frac{PIafter}{PIbefore}$$
$$= \frac{Qf /(Ps - Pwf)after}{Qf /(Ps - Pwf)before}$$

$$= \frac{430/(818-150)}{160/(818-110)}$$

$= 2.85$

Inflow Performance Relationship (IPR) Calculation

Inflow performance relationship (IPR) is curved, expressing how the formation capability to produce fluid through the relationship between the rate of production against bottom hole pressure. The method used in this calculation is the Standing-Harrison method that considers skin and flows efficiency (FE) (Beggs, 1991). The calculation step regarding the IPR calculation on TM#2 as follows:

IPR Before Fracturing (Standing's Method)

1. Calculate skin factor (Darcy Equation)

$$Qo = \frac{0{,}00708\ x\ k\ x\ h\ x\ (Pr-Pwf)}{\mu o\ x\ Bo\ x\ \ln\left(\frac{re}{rw}\right)+S}$$

$$155.74 = \frac{0{,}00708\ x\ 30\ x\ 40\ x\ (818-110)}{3{,}4\ \ x\ 1{,}15\ x\ \ln\left(\frac{570}{0{,}3}\right)+S}$$

S = 9.1 (indicated formation damaged)

2. Calculate FE (flow efficiency)

$$FE = \frac{\ln(0.472\ x\ \left(\frac{re}{rw}\right))}{\ln\left(0.472\ x\ \left(\frac{re}{rw}\right)\right)+S}$$

$$= \frac{\ln(0.472\ x\ \left(\frac{570}{0.3}\right))}{\ln\left(0.472\ x\ \left(\frac{570}{0.3}\right)\right)+9.1\ )} = 0.427$$

3. Calculate Pwf' (Pwf that affected by skin)

Pwf' = Ps-((Ps-Pwf) x FE))
= 818-((818-110) x 0.427)
= 515.68 psig

4. Calculate $Qo/Qmax_{@FE=1}$

$$Qo/Qmax_{FE=1} = 1\text{-}0.2\ \left(\frac{Pwf'}{Ps}\right) - \left(\frac{Pwf'}{Ps}\right)^2$$

$$= 1\text{-}0.2\left(\frac{516.68}{818}\right) - \left(\frac{516.68}{818}\right)^2$$

= 0.55 bopd

5. Calculate $Qmax_{@FE=1}$

$$Qmax_{@FE=1} = \frac{Qo}{Qo/Qmax\ FE=1}$$

$$= \frac{155.74}{0.55} = 279.79 \text{ bopd}$$

6. Calculate $Qmax_{@FE=0.427}$ in assumption of Pwf = 0 psig (Pwf' = 468.19 psig)

$$Qo_{max\ FE=0.427} = Q_{max\ FE=1}\ x\ (1\text{-}0.2\ \left(\frac{Pwf'}{Ps}\right) - \left(\frac{Pwf'}{Ps}\right)^2)$$

$$= 279.79\ x\ (1\text{-}0.2\left(\frac{468.19}{818}\right) - \left(\frac{468.19}{818}\right)^2$$

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= 174.43 bopd.

Therefore, make several assumptions toward value of pwf and pwf' in range of 0-818 psig, then calculated Qo.

IPR After Fracturing (Harrison's Method)

Harrison's IPR Method actually was a modification for Standing's IPR equation. This equation is appropriate used when the value of FE is highly positive and Pwf' is negative(6). The further technical reason if we use Standing's IPR in this condition, it will generate an odd curve of IPR that obviously isn't a representative of IPR from well TM#2. For the steps of calculation as below:

1. Calculate skin factor (Cinco-Ley, Samaniego & Dominiquez)
   After fractured the value of skin is defined through:
   Skin = -ln (rw'/rw)
   For the rw'(fractured rw) is defined through:
   rw'= 0.19 x Xf
   Where the 0.19 is obtained through Chart(Cinco-Ley, Samaniego & Dominiquez) in Figure 9 and for the Xf is obtained through iteration trial error PKN 2D above.
   rw' = 0.19 x 229.516ft
   = 25.86 ft
   Then skin after = -ln(25.86/0.3)
   = -4.45 (Indicated stimulation or improvement)

2. Calculated Flow Efficiency (FE)

$$FE = \frac{Pr - Pwf - \Delta Ps}{Pr - Pwf}$$

$$\Delta Ps = \frac{141.2\ x\ Qx\ Bo\ x\ \mu o}{k \times h} \times S$$

$$= \frac{141.2\ x\ 430\ x\ 1.15\ x\ 3.4}{30 \times 40} \times (-4.45)$$

$$= -880.35$$

$$\text{Then, FE} = \frac{818 - 150 - (-880.35)}{818 - 150} = 2.31$$

3. Calculate Pwf' (Pwf affected by skin)

   Pwf' = Ps-((Ps-Pwf) x FE))

   = 818-((818-150) x 2.31)

   = -730.35 psig

4. Calculate Qo/Qmax $_{@FE=1}$

$$Qo/Qmax_{@FE=1} = 1.2 - (0.2 \times EXP(1.792 \times (\frac{Pwf'}{Ps})))$$

$$= 1.2 - (0.2 \times EXP(1.792 \times \frac{-730.35}{818})))$$

$$= 1.15 \text{ bopd}$$

5. Calculate Qmax $_{@FE=1}$

$$Qmax_{@FE=1} = \frac{Qo}{Qo/Qmax\ FE=1}$$

$= \frac{401.62}{1.15}$ = 346.33 bopd

6. Calculate $Qmax_{@FE=2.31}$ in assumption of Pwf = 0 psig (Pwf' = -1078.03 psig)

$Qo_{max\ FE=2.31} = Q_{max\ FE=1}$ x 1.2-(0.2 x EXP(1.792 x ($\frac{Pwf'}{Ps}$)))

= 346.33 x 1.2 – (0.2 x EXP(1.792 x ($\frac{-1078.03}{818}$)))

= 409.07 bopd.

Therefore, make several assumptions toward value of Pwf' in range of 0-818 psig, then calculated Qo. As the supporting evidence, will be shown the historical oil production as shown in Figure 10. For the IPR result shown in Table 6 and for IPR curve will be shown Figure 11.

Table 6. IPR Calculation

Pwf, psig	Before Frac		After Frac	
	Pwf', psig	Qo, bopd	Pwf' , psig	Qo, bopd
0	468.20	174.44	-1078.03	409.08
50	489.58	166.12	-962.14	407.19
100	510.96	157.50	-846.24	404.76
150	532.34	148.58	-730.35	401.62
200	553.72	139.35	-614.46	397.58
250	575.11	129.81	-498.56	392.37
300	596.49	119.97	-382.67	385.65
350	617.87	109.82	-266.77	376.99
400	639.25	99.37	-150.88	365.83
450	660.63	88.61	-34.98	351.45
500	682.01	77.54	80.91	332.90
550	703.39	66.17	196.81	309.00
600	724.78	54.49	312.70	278.19
650	746.16	42.51	428.59	238.47
700	767.54	30.22	544.49	187.27
750	788.92	17.62	660.38	121.28
800	810.30	4.72	776.28	36.21
818	818.00	0.00	818.00	0

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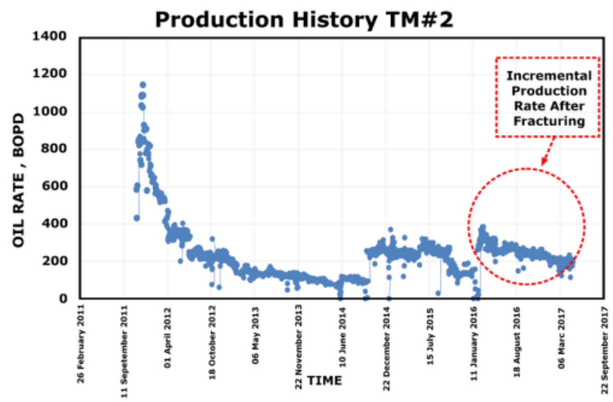

Figure 10. Production History of Well TM#2

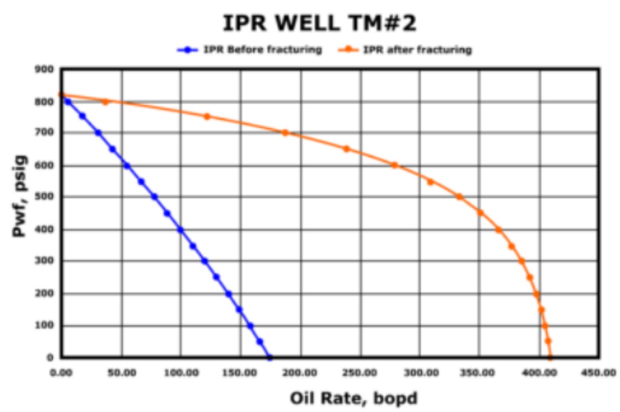

Figure 11. IPR Curve of Well TM#2 Before and After Fracturing

Furthermore, this method is simply answering the problem that already happened in forecasting about how the value of incremental production after fracturing. The problem that commonly happening such as over sizing or lower sizing pump setting. The geometry model from PKN 2D tendency give a small geometry result than fracCADE 3D result. This is caused by the PKN 2D basically calculated based on mathematically concept, instead the fracCADE 3D calculated geometry model based on several considerations such as pressure behaviour, fluid properties, and reservoir properties. But the combination PKN 2D and Cinco-Ley, Samaniego & Dominguez Chart's successfully accomplished the approximation value in order for forecasting production after fracturing based on this sample case. The trial error and iteration flow-step on PKN 2D calculation above start from value 49,07 m. This value is used to be start point in case could penetrate the interest zone as far as 49.07 m. After reached error value less than 0.0001 the result are Half Length (X)= 69.95671953 m = 229.516 ft. Width in front of perforation W(0) = 0.071747 m = 2.824 inch. Average width (w) = 0.0450572 m = 1.7739 inch. Fractured height (h) = 38.1 m = 125 ft (software result) and Pnet = 1736 psi. Pnet is defined as the pressure that make fluid available for propagating the fracture and producing width. The next step, find the effective well radius (rw') by make an intersection perpendicularly in line X for Fcd towards line Y for rw'/Xf through Cinco-Ley, Samaniego and Dominguez. From above chart, the value for rw'/Xf is 0.19. Then this value proceeding to the calculation of J/Jo (PI after/before fracturing) comparison through the three concepts such from software, PKN 2D method, and the actual of production history data. From the three calculations we could see clearly that the result from J/Jo in PKN 2D method successfully reached the approximation PI comparison prediction from actual production data. This clearly stated this concept successfully applied. The next step is IPR curve using the Standing-Harrison equation. This IPR method, consider the skin factor and FE as the basic influence that impact to the production performance.

As stated above, that hydraulic fracturing could be a best option for skin-bypass to improve the damaged zone in reservoir.

CONCLUSIONS

Geometry model and iteration of PKN 2D method generated a small fractured geometry model rather than software fracCADE modelling. This is caused the PKN 2D method just an approximation based on mathematically model without other consideration such as rock properties, pressure maintenance, and fluids properties behaviour. The cooperation between PKN 2D method and Cinco-Ley, Samaniego & Dominguez concept successfully reached for the post hydraulic fracturing production forecast in case well TM#2 by generated a closer result to PI comparison through actual production history. This concept could be appropriate to be used as a quick look measurement for production scenario in order to solve the problem in over sizing or lower sizing pump setting in artificial lift method.

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NOMENCLATURE

n' base gel = Power law index
K' base gel = Flow behaviour index
Qi = Rate fluid injection, bpm
T_t = Total treatment time, minutes
S_p = Spurt loss, gal/100ft^2
C_L = Coefficient Leak-Off, ft/√min
$\bar{w}$ = Average fractured width
h_f = Height of fractured, ft
X_f = Half length of fractured
W(o) = Width in front of perforation, inch
E' = Plain strain modulus, psi
β = Coefficient for Equation-4 in PKN 2D
P_{net} = Pressure Net, psi
PI = Productivity Index, bbl/psi
J/Jo = PI after frac/PI before frac
Wkf = Fractured Conductivity
ki = Initial permeability, mD
re = Drainage radius of reservoir, ft
rw = Well radius, ft
Ql = Rate fluid production, BFPD
Qotest = Rate oil production, BOPD
Qw = Rate water production, BWPD
Qg = Rate gas production, MSCF
WC = Water cut, %
Pr = Reservoir pressure, psi
Pwf = Bottom hole flowing pressure, psi
Pb = Bubble point pressure, psi
Bo = Formation Factor Volume Oil, BBL/STB
μo = Oil viscosity, cp
Fcd = Fractured conductivity dimensionless
S = Skin factor
FE = Flow efficiency, fraction
ΔPs = Total Skin
Pwf' = Pwf affected by skin factor

APPENDIX

Table 7. Final Pad Scenario for Main Fracturing

Job Execution									
Step Name	Step Fluid Name (gal)	Cum Fluid Vol (gal)	Step Slurry Vol (bbl)	Cum Slurry Volume (bbl)	Step Prop (lb)	Cum Prop (lb)	Avg Surface Pressure (psig)	Step Time (min)	Cum Time (min)
PAD	28140	28140	670	670	0	0	2320	37.2	37.2
1 PPA	2016	30156	49.1	719.1	1008	1008	2373	2.7	39.9
2 PPA	2184	32340	54.3	773.4	2184	3192	2371	3	42.9
3 PPA	2310	34650	59.8	833.2	4620	7812	2371	3.3	46.2
4 PPA	2900	37550	76.8	910	8700	16512	2383	4.3	50.5
5 PPA	3500	41050	95.7	1005.7	14000	30512	2431	5.3	55.8
6 PPA	3780	44830	106.7	1112.4	18900	49412	2600	5.9	61.7
FLUSH	2073	46903	49.3	1161.7	0	49412	2586	2.7	64.4

Table 8. Fractured Geometry Data

Proppant	UoM	Pleliminary Design	Re-design	Post Job Estimated
Fracture Properties				
Model Used in Analysis		P3D	P3D	P3D
Propped Fracture Half Length	ft	158.4	267.4	263.1
Fracture Height	ft	125	102.7	107.8
Average Propped Width	in	0.214	0.123	0.11
Fracture Conductivity	md-ft	10290	6908	6917
Net Pressure	psi	1370	1117	904

Table 9. Zone Geomechanic Data

Formation Mechanical Properties							
Zone Name	Top TVD (ft)	Zone Height (ft)	Frac Grad. (Psi/ft)	Insitu Stress (psi)	Young's Modulus (psi)	Poisson's Ratio	Toughness (psi.in0.5)
Clean-Sandstone	5165.4	8.4	0.701	3623	3.805E+6	0.20	1200
Clean-Sandstone	5173.8	5.6	0.713	3690	1.579E+6	0.25	700
Clean-Sandstone	5179.4	5.3	0.712	3691	1.729E+6	0.25	700
Clean-Sandstone	5184.7	4.7	0.727	3771	2.063E+6	0.25	700
Clean-Sandstone	5189.3	7.5	0.733	3808	2.479E+6	0.25	700
Clean-Sandstone	5195.8	4.5	9.762	3963	3.525E+6	0.25	700
Shale	5201.3	3.4	0.802	4174	3.230E+6	0.35	1000
Shale	5204.7	3.1	0.839	4366	4.494E+6	0.35	1000
Shale	5207.8	3.5	0.832	4334	4.494E+6	0.35	1000
Shale	5211.3	3.2	0.823	4291	4.494E+6	0.35	1000
Shale	5214.5	6.1	0.823	4162	2.994E+6	0.35	1000
Shale	5220.5	3.6	0.787	4108	2.163E+6	0.35	100
Shale	5224.1	3.7	0.788	4117	2.351E+6	0.35	100
Shale	5227.8	1.	0.799	4179	3.026E+6	0.35	1000

Table 10. Fluid Behaviour Data

Parameters	Type 1	Type 2
Fluid Name	Brine	YF 130 HTD
C_L (ft/√min)	20E-2	35E-4
Spurt (gal/100 ft^2)	0.0	0.0
Temperature (^{0}F)	250	250
Behaviour Index (N')	0.2	0.4
Consist Index (K')	4.84E-6	3.5E-1

Table 11. Value of β[4)]

ß	Exp ($ß^2$) erfc ß + (2ß/√π) - 1	ß	Exp ($ß^2$) erfc ß + (2ß/√π) - 1	ß	Exp ($ß^2$) erfc ß + (2ß/√π) - 1
0.00	0.00000	0.88	0.45571	3.30	2.88766
0.02	0.00039	0.90	0.47207	3.40	2.99602
0.04	0.00155	0.92	0.48858	3.50	3.10462
0.06	0.00344	0.94	0.50523	3.60	3.21343
0.08	0.00603	0.96	0.52201	3.70	3.32244
0.10	0.00929	0.98	0.53892	3.80	3.43163
0.12	0.01320	1.00	0.55596	3.90	3.54099
0.14	0.01771	1.05	0.59910	4.00	3.65052
0.16	0.02282	1.10	0.64295	4.10	3.76019
0.18	0.02849	1.15	0.68746	4.20	3.87000
0.20	0.03470	1.20	0.73259	4.30	3.97994
0.22	0.04142	1.25	0.77830	4.40	4.09001
0.24	0.04865	1.30	0.82454	4.50	4.20019
0.26	0.05635	1.35	0.87127	4.60	4.31048

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0.28	0.06451	1.40	0.91847	4.70	4.42087
0.30	0.07311	1.45	0.96611	4.80	4.53136
0.32	0.08214	1.50	1.01415	4.90	4.64194
0.34	0.09157	1.55	1.06258	5.00	4.75260
0.36	0.10139	1.60	1.11136	5.20	4.97417
0.38	0.11158	1.65	1.16048	5.40	5.19602
0.40	0.12214	1.70	1.20991	5.60	5.41814
0.42	0.13304	1.75	1.25964	5.80	5.64049
0.44	0.14428	1.80	1.30964	6.00	5.86305
0.46	0.15584	1.85	1.35991	6.20	6.08581
0.48	0.16771	1.90	1.41043	6.40	6.30874
0.50	0.17988	1.95	1.46118	6.60	6.53184
0.52	0.19234	2.00	1.51215	6.80	6.75508
0.54	0.20507	2.05	1.56334	7.00	6.97845
0.56	0.21807	2.10	1.61472	7.20	7.20195
0.58	0.23133	2.15	1.66628	7.40	7.42557
0.60	0.24483	2.20	1.71803	7.60	7.64929
0.62	0.25858	2.25	1.76994	7.80	7.87311
0.64	0.27256	2.30	1.82201	8.00	8.09702
0.66	0.28675	2.35	1.87424	8.20	8.32101
0.68	0.30117	2.40	1.92661	8.40	8.54508
0.70	0.31580	2.45	1.97912	8.60	8.76923
0.72	0.33062	2.50	2.03175	8.80	8.99344
0.74	0.34564	2.60	2.13740	9.00	9.21772
0.76	0.36085	2.70	2.24350	9.20	9.44206
0.78	0.37624	2.80	2.355001	9.40	9.66645
0.80	0.39180	2.90	2.45690	9.60	9.89090
0.82	0.40754	3.00	2.56414	9.80	10.11539
0.84	0.42344	3.10	2.67169	10.00	10.33993
0.86	0.43950	3.20	2.77954		

For value of ß>4, exp (ß^2) erfc ß ≈ (1/(ß/√π))

Table 12. Trial Error PKN 2D Method

Itr, m	Xf(itr) ,m	w(o), m	w, m	b	exp(b2)erfc(b)	Xf (itr+1), m	error
1	49.07	0.063212135	0.039697221	0.807998453	0.383753	77.2302114	28.1602114
2	77.2302114	0.07432712	0.046677431	0.687169199	0.2911565	68.89834263	-8.331868769
3	68.89834263	0.071357679	0.044812622	0.715764696	0.3092165	70.24871042	1.350367794
4	70.24871042	0.071854055	0.045124346	0.710820114	0.305559	69.90067038	-0.348040046
5	69.90067038	0.071726711	0.045044375	0.712082104	0.3065026	69.99226714	0.091596758
6	69.99226714	0.071760265	0.045065446	0.71174915	0.30620272	69.95649736	-0.035769772
7	69.95649736	0.071747165	0.04505722	0.711879102	0.306272213	69.95960056	0.003103194
8	69.95705569	0.07174737	0.045057348	0.711877073	0.306259702	69.95694221	-0.000113486
9	69.95671953	0.071747246	0.045057271	0.711878295	0.306259087	69.95668178	-3.77483E-05
10	69.95671953	0.071747246	0.045057271	0.711878295	0.306259087	69.95668178	-3.77483E-05

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